

Assignatura: Computational mechanics

Estudiant/a: _____

Data: 04/05/2019

① We have $\underline{\underline{\sigma}} = \eta \underline{\underline{\epsilon}}^{\text{dev}}$!



(a) The constitutive law: $\underline{\underline{\sigma}} = \underline{\underline{f}}(\underline{\underline{\epsilon}})$ (relation between $\underline{\underline{\sigma}}$ and $\underline{\underline{\epsilon}}$)

$$\underline{\underline{\epsilon}} = \nabla^S \underline{u} = \frac{1}{2} (\nabla u + (\nabla u)^T)$$

$$\epsilon_{ij} = \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \frac{1}{2}$$

} Small strain tensor

In our case $\underline{\underline{f}}(\underline{\underline{\epsilon}}) = \underline{\underline{\sigma}} = \eta \underline{\underline{\epsilon}}$

$$\nabla^S \underline{u}^h \underline{\sigma}^h = \{ \underline{\epsilon}^h \}^T \{ \underline{\sigma}^h \} = \begin{pmatrix} \frac{\partial u_x^h}{\partial x} \\ \frac{\partial u_y^h}{\partial y} \\ \frac{\partial u_z^h}{\partial z} \\ \frac{\partial u_x^h}{\partial y} + \frac{\partial u_y^h}{\partial x} \\ \frac{\partial u_x^h}{\partial z} + \frac{\partial u_z^h}{\partial x} \\ \frac{\partial u_y^h}{\partial z} + \frac{\partial u_z^h}{\partial y} \end{pmatrix}^T \begin{pmatrix} \sigma_x \\ \sigma_y \\ \sigma_z \\ \tau_{xy} \\ \tau_{xz} \\ \tau_{yz} \end{pmatrix}$$

$$\sum_{\forall u_i} u_i \left[\int \rho \frac{d^2 u_i}{dt^2} N_i(x) N_i(x) d\Omega + \int \underline{B}_i^T \underline{\underline{C}} \underline{B}_i d\Omega \right] = \int \rho b_i N_i + \int t_i N_i ds$$

$$\Rightarrow \int \rho N_i(x) N_j(x) d\Omega \frac{d^2 u_j}{dt^2} + \underbrace{\int \underline{B}_i^T \underline{\underline{C}} \underline{B}_j d\Omega}_{K_{ij}^e} u_j = f_i$$

↑
Linear elasticity

$$K_{ij}^e = \int_{\Omega} \underline{B}_i^T \underline{\underline{C}} \underline{B}_j d\Omega \quad \times$$

$$(b) \quad \{ \varepsilon(u^h) \} = \sum_{j=0}^8 \begin{pmatrix} \partial_x N_j & 0 & 0 \\ 0 & \partial_y N_j & 0 \\ 0 & 0 & \partial_z N_j \\ \vdots & \vdots & \vdots \end{pmatrix} \begin{pmatrix} u_x \\ u_y \\ u_z \end{pmatrix} = \sum_{i=1}^8 u_i \mathbf{B}_i \mathbf{T}_i$$

8×3

We have $3 \times (n+1) = 3(8+1) = 27$ equations $\dim(K) = 27$.

↑
?

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② We have $K = \frac{E}{h} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$ $M = \frac{hp}{6} \begin{bmatrix} 2 & 1 \\ 1 & 2 \end{bmatrix}$

(a) We know that the eigen-frequencies ω_i are $\omega_i^2 = \lambda_i$ where $M^{-1}Ku = \lambda u$

Compute $M^{-1}K$:

$$M^{-1} = \frac{6}{3hp} \begin{bmatrix} 2 & -1 \\ -1 & 2 \end{bmatrix} = \frac{2}{hp} \begin{bmatrix} 2 & -1 \\ -1 & 2 \end{bmatrix}$$

$$M^{-1}K = \frac{2}{hp} \frac{E}{h} \begin{bmatrix} 2 & -1 \\ -1 & 2 \end{bmatrix} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} = \frac{2E}{ph^2} \begin{pmatrix} 3 & -3 \\ -3 & 3 \end{pmatrix}$$

Now, find eigenvalues: for

$$\begin{vmatrix} x-3 & -3 \\ -3 & x-3 \end{vmatrix} = (x-3)^2 - 9 = 0 \iff \begin{cases} x=0 \\ x=6 \end{cases}$$

Therefore $\omega_1 = \sqrt{0 \cdot \frac{2E}{ph^2}} \Rightarrow \boxed{\omega_1 = 0}$

$$\omega_2 = \sqrt{6 \cdot \frac{2E}{ph^2}} \Rightarrow \boxed{\omega_2 = \frac{1}{h} \sqrt{12E/p}}$$
 ✓

(b) Now we have $\underline{M}^L = \frac{hp}{6} \begin{bmatrix} 3 & 0 \\ 0 & 3 \end{bmatrix}$

Compute $(M^L)^{-1}K$:

$$(M^L)^{-1} = \frac{2}{3hp} \begin{pmatrix} 3 & 0 \\ 0 & 3 \end{pmatrix}$$

$$(M^L)^{-1}K = \frac{2E}{3h^2p} \begin{pmatrix} 3 & -3 \\ -3 & 3 \end{pmatrix}$$

The eigen-values are $\begin{cases} x=0 \\ x=6 \end{cases}$ ✓

But now, we have:

$$\omega_1 = \sqrt{0 \cdot \frac{2E}{3h^3\rho}} = 0 \Rightarrow \boxed{\omega_1 = 0}$$

$$\omega_2 = \sqrt{6 \cdot \frac{2E}{3h^3\rho}} \Rightarrow$$

$$\boxed{\omega_2 = \frac{2}{h} \sqrt{\frac{E}{\rho}}} \quad \checkmark$$

(c) We want Δt_{crit} minimum, because we want a minimum critical time-step difference. ~~No!~~

In case (a), we have $\omega_{z(a)} = \frac{1}{h} \sqrt{12 \frac{E}{\rho}} = \frac{2}{h} \sqrt{3 \frac{E}{\rho}}$

In case (b) we have $\omega_{z(b)} = \frac{2}{h} \sqrt{\frac{E}{\rho}}$

$\Rightarrow \omega_{z(a)} > \omega_{z(b)}$ and in our case we want the maximum because $\frac{1}{\omega_{\text{max}}}$ be minimum.

[Therefore, the M^L is better. \checkmark]

(d) If h is less, ω_2 will increase $\Rightarrow \rho$ is going to affect to the stability. ~~X~~

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③ ¹⁰ We have a shear stress $\sigma = \begin{pmatrix} 0 & \tau & 0 \\ \tau & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$

And the material follows a Von Mises plasticity criteria.

This implies that $f(\sigma) = \sqrt{3}J_2 - \sigma_y$ ✓

And we know that when $f(\sigma) < 0$ we have elasticity
and when $f(\sigma) = 0$ we have plasticity.

We have to compute J_2 .

$$J_2 = \frac{1}{2} \sigma' : \sigma' = \frac{1}{2} \sigma : \sigma - \frac{3}{2} \sigma_m^2 = \frac{1}{3} I_1^2 - I_2 = \tau^2$$

Where $I_1 = \text{tr}(\underline{\sigma})$ and $I_2 = \text{tr}(\underline{\sigma}^2)$

$$I_1 = 0 \quad I_2 = 2\tau^2 \quad \times$$

$$\Rightarrow J_2 = \frac{1}{3} \cdot 0 - 2\tau^2 \Rightarrow J_2 = \cancel{2\tau^2}$$

Now, $f(\sigma) = \sqrt{-2\tau \cdot 3} - \sigma_y = \sqrt{-6\tau} - \sigma_y$

We want $f(\sigma) = 0 \Rightarrow \sqrt{-6\tau} = \sigma_y$

$$\Leftrightarrow -6\tau = \sigma_y^2 \Rightarrow \tau = \frac{\sigma_y^2}{6}$$

This is the maximum shear stress τ .

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Estudiant/a: [REDACTED]

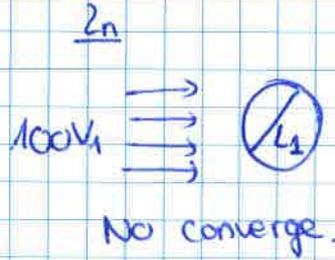
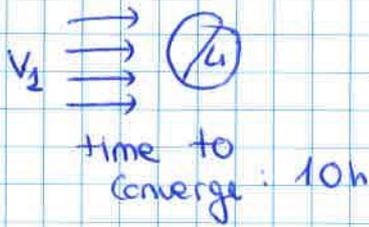
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④

(a) The scheme of the problem is:

⑤0

1st time



In the first time you have a Reynolds number is

$Re_1 = \frac{L_1 v_1}{\nu}$ and in the second case: $Re_2 = 100 Re_1$

The error in the second case may be because the other conditions (except the velocity) are the same.

A fine enough mesh (or adapted to features) is necessary for convergence of a non-linear solver, because we are in Navier-Stokes equation. ✓

The solution is take a mesh with more nodes.
 (+ better initial/guess)

⑤0

(b) Now we have $L_2 = L_1/100$ and $V_2 = 100V_1$

Now, $Re_1 = \frac{L_1 v_1}{\nu}$ and $Re_2 = \frac{L_2 v_2}{\nu} = \frac{100 L_1 v_1 / 100}{\nu} = \frac{L_1 v_1}{\nu}$

$\Rightarrow Re_1 = Re_2$

In this case we don't have a problem with the computation because the Reynolds number is



equal. We can obtain the solution with previous ones.

$$\bar{v}_2 = \begin{pmatrix} 2 \\ 6 \end{pmatrix} \bar{v}_1$$